

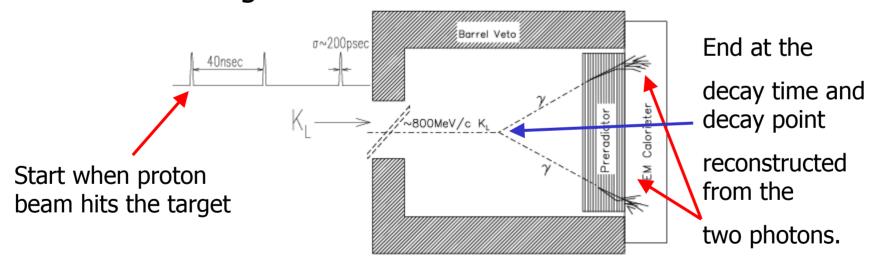


## **KOPIO Specifications** for AGS Performance



# Physics Motivation: Microbunch Width

KOPIO fully reconstructs the neutral Kaon in  $K_L \rightarrow \pi^0 \ v \ \overline{v}$  measuring the Kaon momentum by time-of-flight.



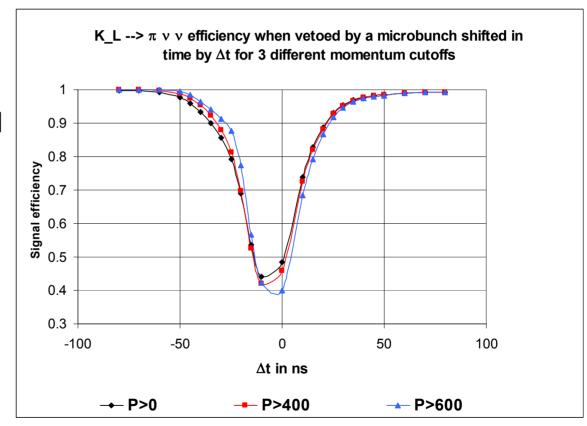
Timing uncertainty due to microbunch width should not dominate the measurement of the kaon momentum; requires RMS width < 300ps



## Physics Motivation: Microbunch Separation

Microbunch separation determined by the length of time required to clear out kaons from the previous microbunch.

Difference in time-of-flight between high momentum and low momentum kaons is ~30 nsec => 40nsec (25MHz)



Signal efficiency drops when neighboring microbunch too close



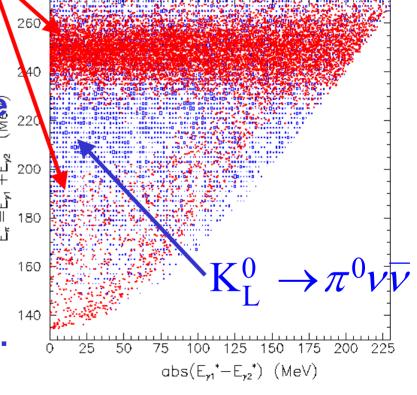
# Separating signal from background

 $K_L^0 \rightarrow \pi^0 \pi^0$ 

$$E_{\pi^0}^*$$
 vs.  $E_{\gamma 1}^* - E_{\gamma 2}^*$ 

Microbunching is crucial to the measurement of the kaon momentum which allows us the kinematic suppression of backgrounds by transforming to the kaon rest frame.

Make cuts on the pion energy and the difference in photon energies in the kaon rest frame.



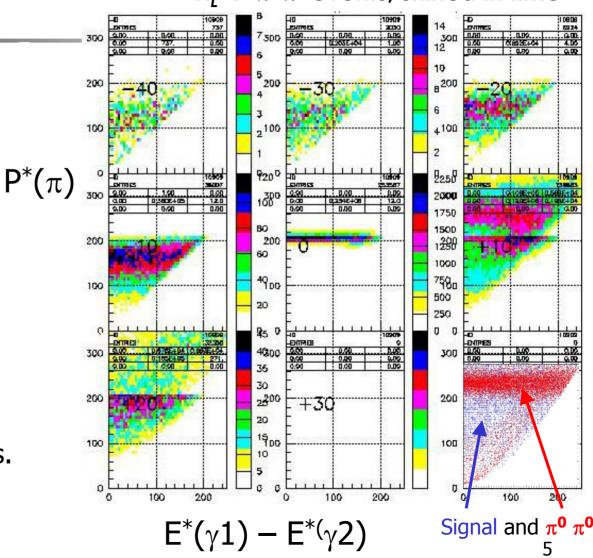
#### Physics Motivation: Interbunch Extinction

Effects of Interbunch Kaons

 $K_L \rightarrow \pi^0 \, \pi^0$  events, shifted in time

Kinematic cuts are used to reduce background due to  $K_I \rightarrow \pi^0 \pi^0$ 

When  $K_L$  does not come from the microbunch, incorrect kinematic fit does not allow for good rejection. Panels show effect of  $K_L$  production at varying interbunch times.





### Physics Motivation: Intensity

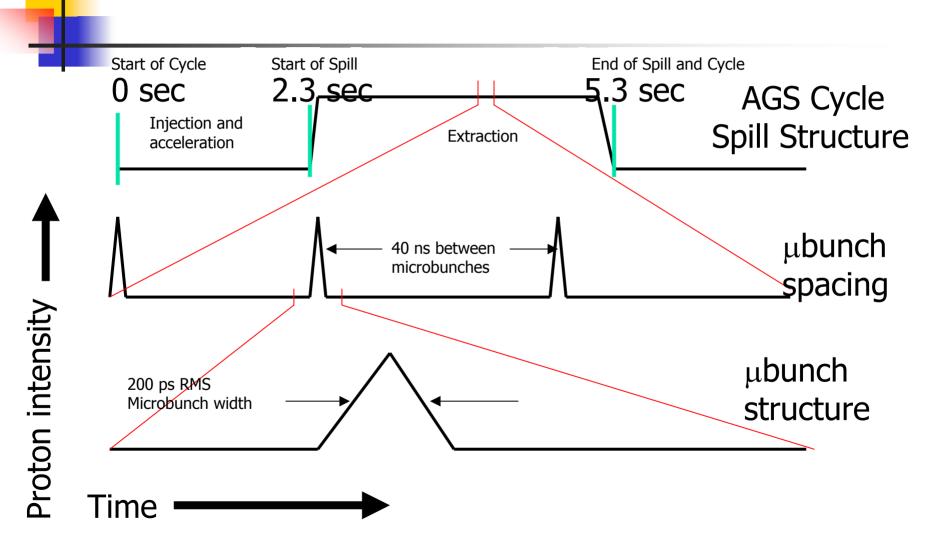
- KOPIO studies the very rare decay  $K_I \rightarrow \pi^0 \, \nu \, \overline{\nu}$  which has a BR =  $3 \times 10^{-11}$ .
- The goal is to collect  $\sim$ 100 events with a S/B > 2/1.
- This requires more than  $1.5 \times 10^{14}$  decays and for cleanliness we want  $\sim 0.5$  decay/spill in the decay region.
- Optimization of duty factor and running time indicates 100Tp/spill.



## **KOPIO** Beams requirements

- Spill length with 100TP of ~3 seconds.
- Number of  $K_{L}$  decays per microbunch: 3.57
  - Yields ~0.5 *K*, decay in 10 < Z < 14 meters
  - Both are a flat optimum
- Variation of intensity between microbunches only impacts total run time (duty factor)
- Microbunch rms < 300psec (goal 200psec)</li>
- Number of protons outside microbunches
  - < 10<sup>-3</sup> inside microbunches ( +/- 2 nsec)

#### Time Structure of Beam



#### Microbunching the AGS Beam

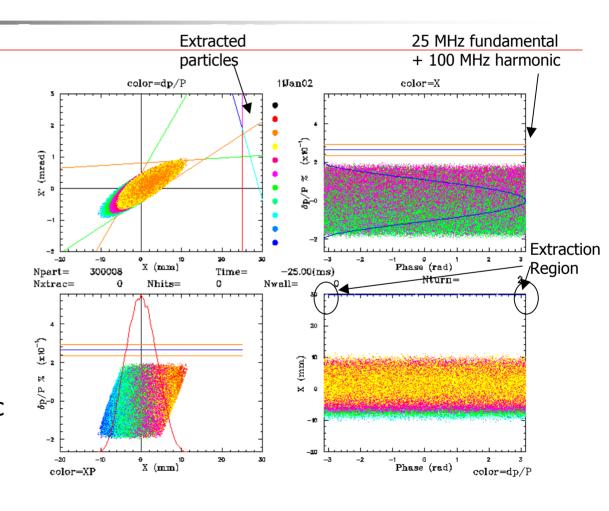
Simulation of the extraction process for 25+100 MHz RF cavities.

Impose a high frequency longitudinal oscillation on the beam.

Slowly bring the beam into resonance  $(8^2/_3)$  with RF.

Beam is forced through the narrow phase region between the RF buckets.

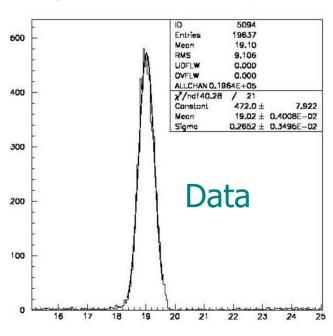
Adding the 100MHz harmonic cavity sharpens up the phase region in resonance.



## Test Beam Results: Microbunch Width

#### Data

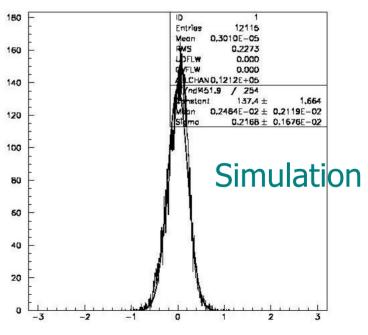
93 MHz cavity at 22 kV gave  $\sigma = 240$  ps.



Microbunch time, in ns

#### Simulation

93 MHz cavity at 22 kV gave  $\sigma = 217$  ps.



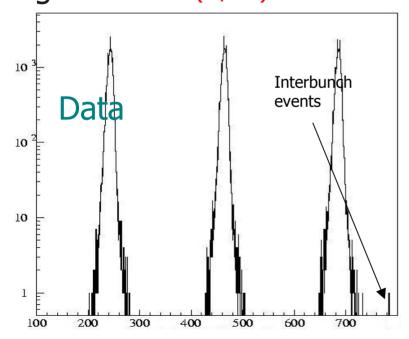
Microbunch time, in ns

#### Test Beam Results: Interbunch Extinction



#### Data

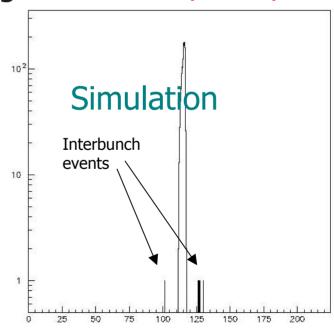
4.5 MHz cavity at 130 kV gave  $\varepsilon = 8 (+/-6) \times 10^{-6}$ 



Microbunch time, in ns

#### Simulation

4.5 MHz cavity at 130 kV gave  $\varepsilon = 1.7 \ (+/- 0.9) \times 10^{-3}$ .



Microbunch time, in ns

#### New Hardware Required: RF

#### Provide KOPIO microbunching:

- Add a 25 MHz 150 kV RF cavity to AGS Ring to provide the 40 ns microbunch spacing and preliminary microbunch width structure.
- Add a 100 MHz 150 kV harmonic RF cavity "afterburner" for very narrow microbunch width.

#### Specification from physics: Kicker

Current kickers do not provide enough kick to get the beam into equilibrium orbit. We inject at 1.94 GeV with ~2 mrad kick.

New kicker system required to inject beam from Booster into AGS without emittance blow-up. It allows for higher transfer energy at injection, 2 GeV, with lower losses.

Need new Pulse Forming Network (PFN) for faster switching to keep one bunch from interfering with its neighbors.

Must keep from activating the machine and damaging equipment in the AGS and Booster.



Provide high-efficiency high-intensity Injection/Extraction:

- Add magnets to create A10 kicker system.
- Upgrade the F3 kicker for Booster extraction.
- Upgrade the A5 kicker system for AGS injection.



### Summary

- Achieved goals for microbunching
- Understand intensity limitations
- Next tests require hardware (25 MHz and kicker)
- Confidence that AGS can provide the structure and intensity for KOPIO's needs with good interbunch extinction.



## Back-up slides follow:



## Current design: RF

Specification of 25 MHz cavity is well understood. Equipment - TRIUMF

- 25 MHz cavity including prototype, HOM dampers, coupling loop, ceramic window.
- RF Amplifier (including tetrode) and its power supplies (plate, screen, and bias).
- Impedance reduction circuitry to be integrated with cavity and amplifier.
- Mechanical trolley for servicing of amplifier.
- 30 kW dummy load for amplifier tests.
- Ferrite tuner including its power supplies and local control circuitry
- Minimal set of cavity local controls for voltage regulation and tuning





#### Equipment - BNL

- RF Driver to be shipped to TRIUMF
- Fast feedback, integration into main controls, low-level RF for beam control and synchronization.
- Cabling and services.

#### Equipment - Both

- Vacuum pump. Issue: for testing purposes only a turbomolecular pump is needed; but an ion pump is required for AGS operations. Vacuum level at BNL AGS is 10<sup>-7</sup> torr, but for RF testing at TRIUMF, specification is less stringent.
- Water cooling. TRIUMF to provide basic plumbing for c.w. power test.



# RF specifications: 25 MHz cavity

Cavity centre frequency: 24.8694 MHz (67<sup>th</sup> harmonic of revolution frequency).

*Gap voltage*: Design to 300 kV, Expected operating voltage 150 kV.

Mechanical Design: BNL to specify flange-to-flange dimension and lateral space available in AGS tunnel.

Insertion length: 101 in (2.56 m)

Vertical space: down/up 24 in (61 cm)/48 in (122 cm)

Horizontal space: in/out 36 in (91 cm)/48 in (122 cm)

#### RF Mechanical specifications

Coupling loop: solid copper and water cooled.

HOM dampers: copy the BNL 28 MHz designs (high pass filter type) which were fabricated for RHIC by Continental Electronics, but adapted to 25 MHz.

Active impedance reduction by fast feedback (BNL): reduce gap impedance from 1 M $\Omega$  to 10 k $\Omega$ .

Cooling Water: separate cooling water supplies for cavity and power amplifier. Inner and outer conductors of the cavity are water cooled. Water cooling of the cavity is a closed loop system with heat exchanger. Water temperature should be maintained within ±5°F; pressure to be controlled also.

*Dummy load*: This equipment is comprised of a quarter wave transformer (at 25 MHz) from 1 kΩ to 10  $\Omega$  and a water-cooled resistive load.



## RF Power amplifier

Amplifier is to be directly mounted on the cavity. Any length of transmission line between the amplifier and the cavity should be avoided.

The amplifier is coupled to the cavity by an inductive loop.

The amplifier will operate with quiescent plate dissipation of 60 kW (12 kV, 5A).

The cavity power requirement is around 50 kW.

Hence total input power to the amplifier is 110 kW.



## RF Power amplifier

A sliding trolley on rails is to be designed to install and service the amplifier on top of the cavity This is a major mechanical engineering job, and must be consistent with space limitations.

A mechanical system will connect an external low impedance load to the anode circuit of the amplifier when the amplifier is non operational. The impedance transformed to the cavity should be of the same value as with fast feedback, i.e.  $10 \text{ k}\Omega$ .

Passive impedance reduction at fundamental: 40 dB. The power rating of this low impedance anode circuit is to be based on a circulating beam current of up to 1.2 Amp at 25 MHz.



#### **RF Tetrode**

**Tetrode**: Eimac 4CW150,000-V57B For ease of installation and connection, make sure to purchase model with same water jacket dimensions as those of existing RHIC cavity.

*Power supplies*: 480 volt *Universal Voltronics*, 3 phase, 300 Amp/phase was mentioned.



## **RF Tuning**

The accelerating gap dimension is a free parameter for bringing the cavity design frequency down from 28 to 25 MHz.

Fixed tuning: part of the mechanical design and used to compensate for manufacture and assembly tolerances; range to be determined by TRIUMF.

Ferrite tuner: ±10 kHz with resolution of 1%, slew rate up to 1 Hz/millisecond. Ferrite tuner consists of a stripline partially filled with microwave ferrite and coupled to the cavity.

#### **RF Ceramic Window**



An RF window employing a disk ceramic is preferred by BNL. Although a tubular ceramic may be superior with regards to RF characteristics, a disk ceramic window was chosen for mechanical considerations and few failures due to multipacting.

The 18" diameter uncoated ceramic disk window is fabricated without any brazing.

The window is air cooled.





#### **R&D Program at TRIUMF**

Build a model 25 MHz cavity of wood + copper

#### At BNL

- Drawings of BNL standard vacuum flange and seal.
- Engineering note on HOM dampers.
- Alex Zaltsman overseeing RF work in contact with Amiya Mitra at TRIUMF.
- More simulation work required (added processing farm at C-A) to explore need for 100 MHz cavity.



Design of kicker system is still in the early stages.

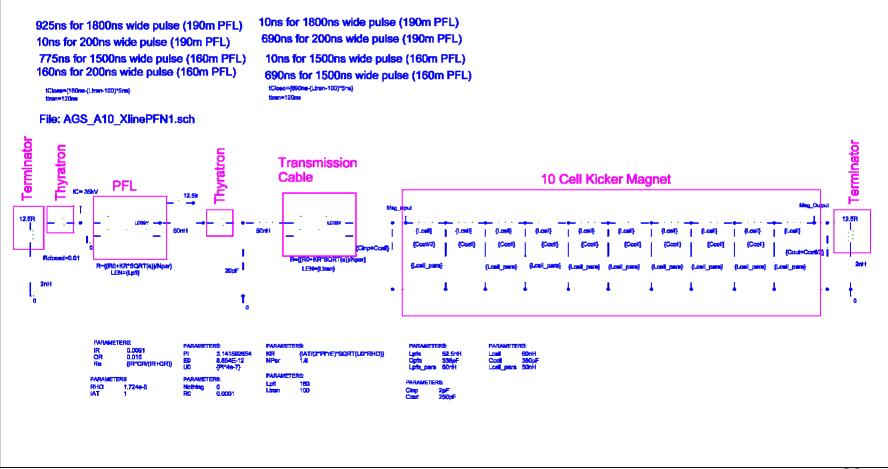
- Upgrade the F3 booster extraction kicker
- Add 2 new design kicker elements at the A10 straight section.
- Possibly replace/upgrade the existing 3 kicker magnets at A5.

## A10 Kicker Parameters

A10 kicker parameters	<b>Specifications</b>
Pulse repetition rate	7.5 Hz
Field uniformity in aperture	±3%
(combined electric & magnetic field)	
Pulse to pulse reproducibility of field	$\pm 1\%$
Maximum flat top duration	1800 ns
Aperture width	127 mm wide
Aperture height	81 mm high
Confirm rise and fall times	100 ns
Rise time definition	3% to 97%
Fall time definition	97% to 3%
Flat top ripple	±3%
Ripple between pulses	±3% of maximum

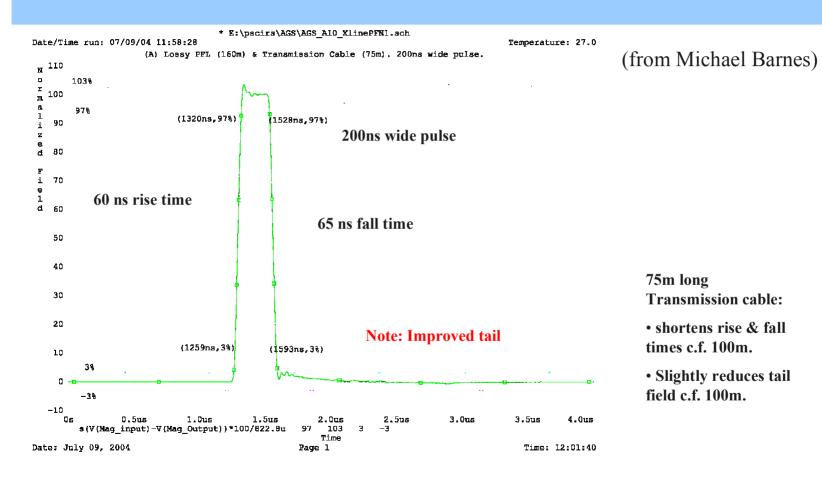
#### Simplified Schematic of AGS A10 Kicker System

(from Michael Barnes)



#### Predicted Field in A10 kicker.

Lossy PFL (160m) & Transmission Cable (75m). 200ns wide pulse. Cout=250pF.



# More A10 Kicker Parameters



A10 kick strength for 2 GeV protons

Charge time for PFL:

Available insertion length at A10:

Vacuum:

Bake-able vacuum tank temp:

Length of cables from Pulse

Forming Line (PFL) to A10 kicker:

**BNL-TRIUMF** interface:

A5 distance between gate valves:

A5 kicker length for 3 magnets:

#### **Specifications**

1.5 mrad

10's of ms

94" between gate valves

10<sup>-7</sup> to 10<sup>-9</sup> Torr

200 deg C

200ft or less to

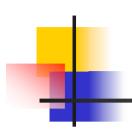
minimize tail of field pulse

TTL and fiber optics to

thyratron trigger

43"

36"



### Even More A10 Kicker Params

#### **A10 kicker parameters**

Saturable ferrite's required on input to kicker magnet.

Length of cables from A10 kicker to terminator

Mount terminator on vacuum tank or use short cables to terminators located in tunnel.

Radiation levels in cables at input and output of kicker appears not to be a problem due to low radiation damage to cables in the AGS tunnel, providing we use polyethylene dielectrics with cable specified for 150kV DC.



#### TRIUMF contributions to Kicker

#### HV portion including:

- Transmission line kicker magnet
- HV Power Supply
- Thyratrons and switch assembly,
- optically isolated thyratron grid drive circuits (e.g. MA2709A from E2V),

PFL cables, HV transmission cables,

Terminating resistors, Vacuum tank

Fast anti-parallel ("clipper") diodes (e.g. EUPEC) with grading capacitors.



#### **BNL** contributions to Kicker

- Controls and timing.
- New A10 building
- New cable runs to A10 as short as possible to minimize tail on field pulse.



- Confirm A10 kick strength (1.5 mrad) for 2 GeV protons.
- Confirm that commercial capacitor charging power supply is to be used for charging PFL
- Confirm absence of beam pipe through kicker aperture.
- Thyratron choice to be determined by TRIUMF
  - (e.g. 2 gap CX1168C)
- Obtain drawings of existing AGS thyratron switch tanks in air
- Beam impedance issues needs better understanding.
- "Pspice" simulation work needs to be completed.

## Space – Testing/Installation

There are plans for limited testing of RF cavities and kickers to be completed at TRIUMF before shipping to BNL, but we need more planning for *in situ* testing at BNL. It must be worked into the overall AGS schedule.



## Safety

"Safety" is a concern in terms of the likelihood of failure of a component in a way that would impact the AGS schedule. The design has been studied to minimize such impacts.

Ease of maintenance and ALARA have been important design criteria.

## Resources

- Injection kicker development at TRIUMF with BNL C-A support
  - Ready to call on CFI funding
- RF design is well suited to TRIUMF and BNL capabilities.



#### Issues

- Fast Feedback for RF power supply.
- Active Impedance reduction for RF.
- Better understanding of Beam Kick provided by A10 design.
- 100 MHz necessity.
- Scheduling.



## Summary

The AGS Mods subsystem is in an advanced state of development.

There are few fundamental uncertainties remaining.

Both TRIUMF and BNL have strong groups ready to do the work.